
Flexión Oblicua

Clase 14
Tensiones



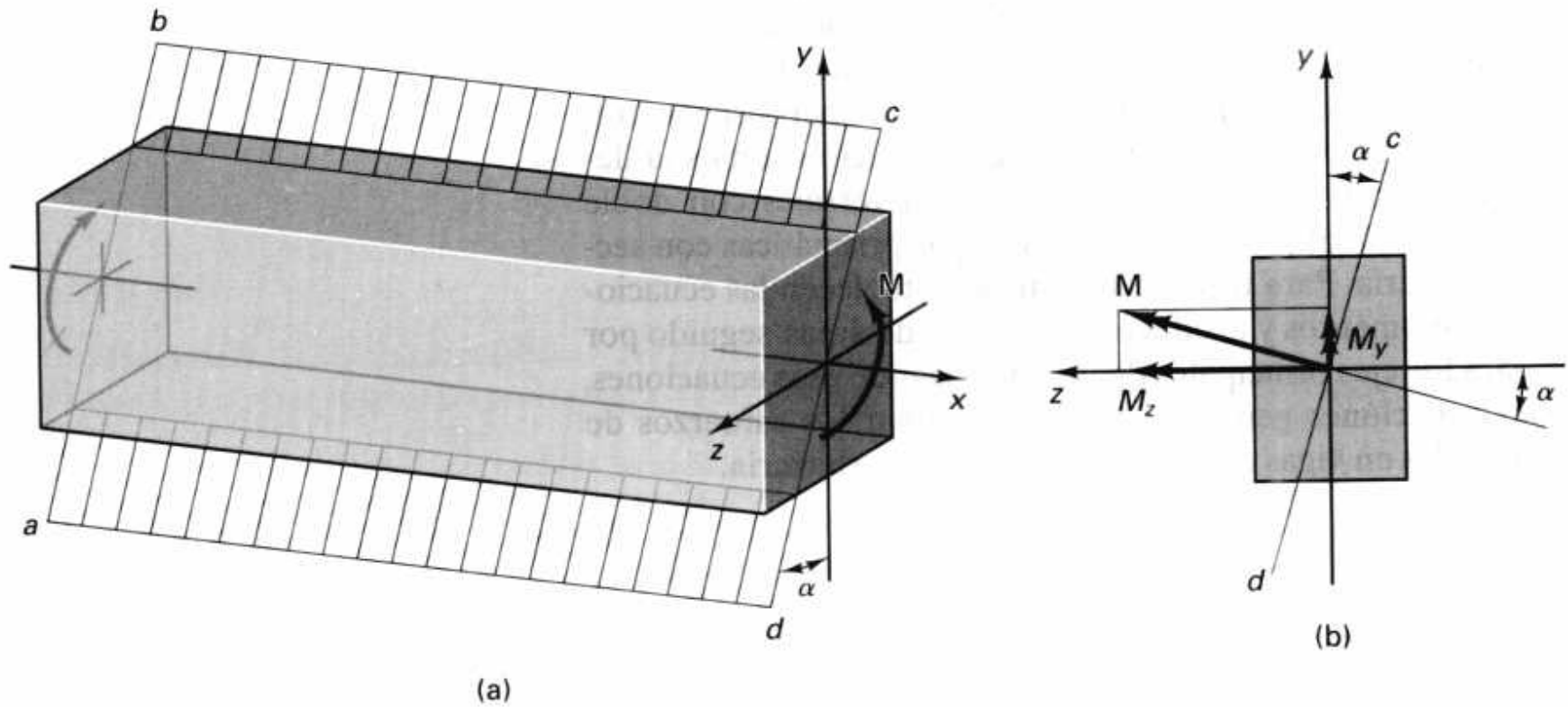


Fig. 9-1 Flexión asimétrica de una viga con sección transversal doblemente simétrica.

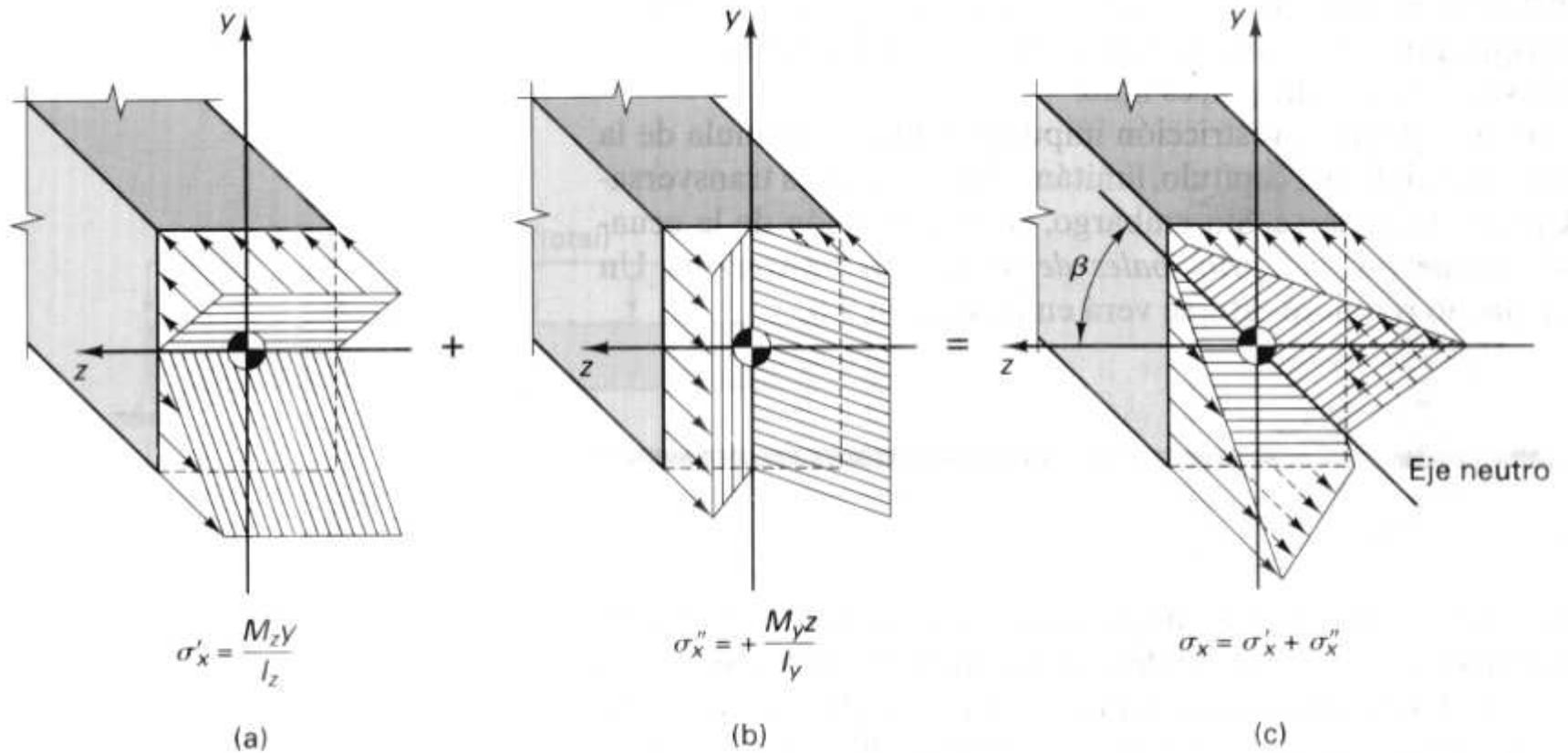
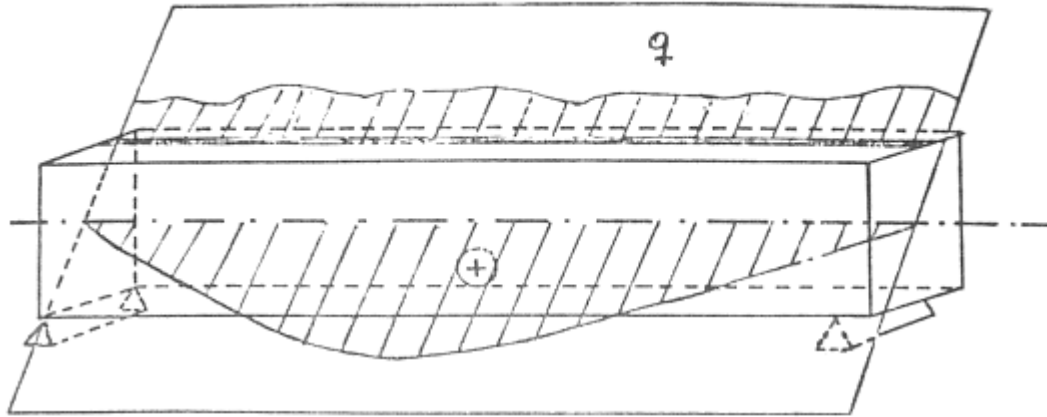
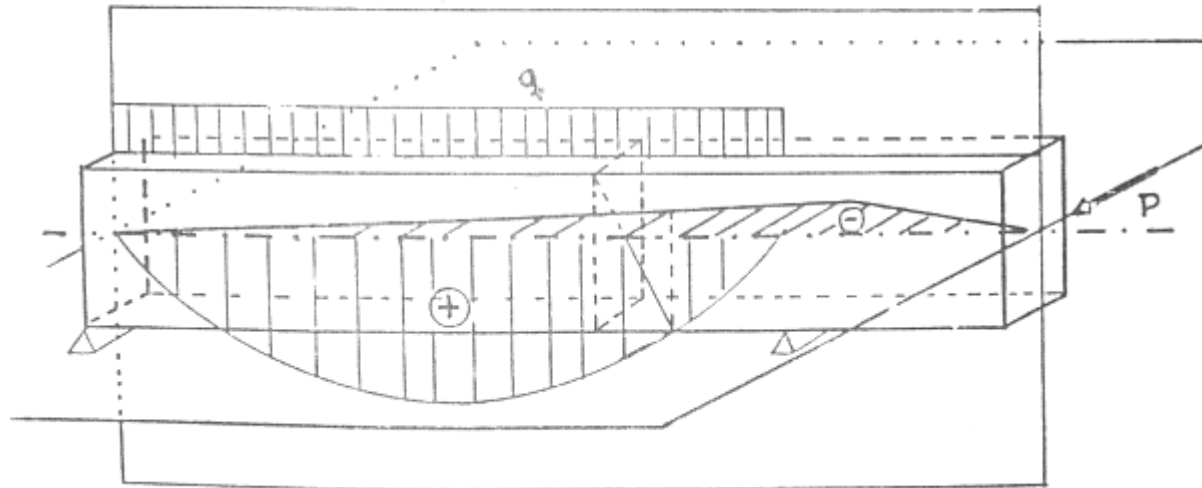


Fig. 9-2 Superposición de esfuerzos elásticos de flexión.

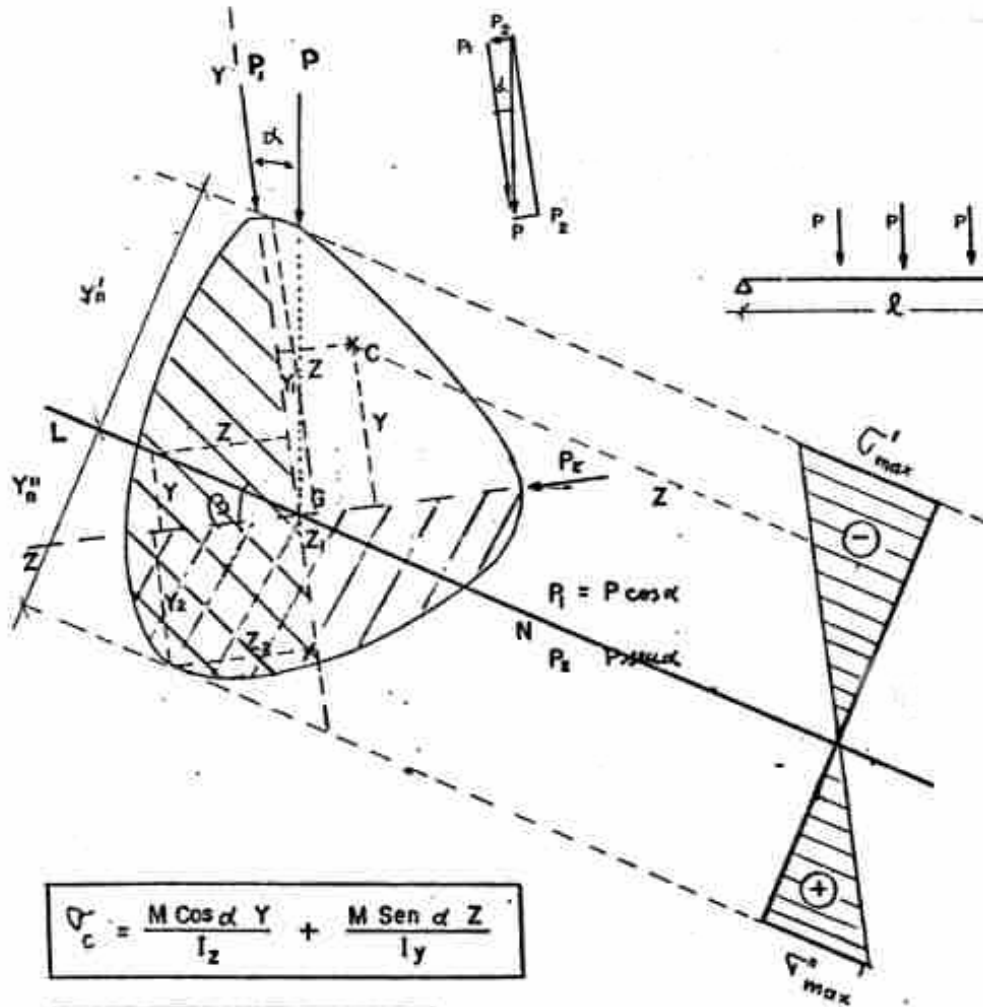
FLEXION DESVIADA



FLEXION DOBLE



FLEXIÓN OBLICUA



$$\sigma_c = \frac{M \cos \alpha \cdot Y}{I_z} + \frac{M \sin \alpha \cdot Z}{I_y}$$

$$\sigma_c = \frac{M_y \cdot Y}{I_z} + \frac{M_z \cdot Z}{I_y}$$

POSICION DE LA LINEA NEUTRAL:

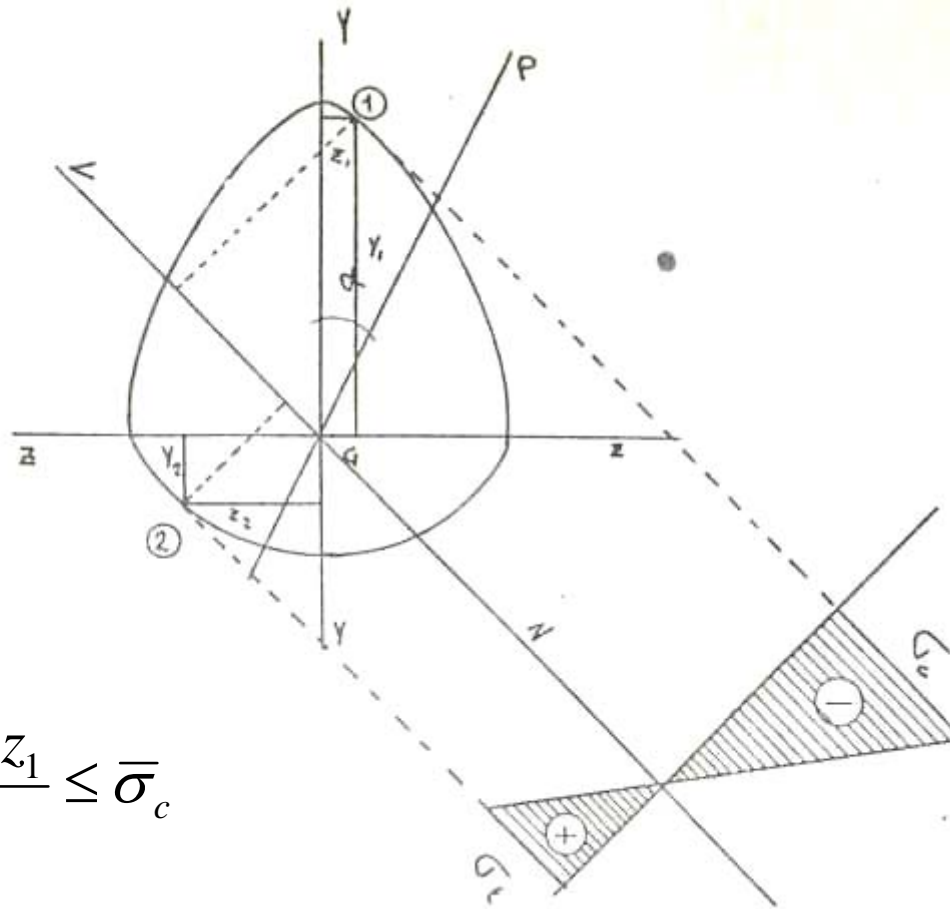
$$\frac{M \cos \alpha \cdot Y}{I_z} + \frac{M \sin \alpha \cdot Z}{I_y} = 0$$

$$\frac{Y}{Z} = - \frac{\sin \alpha}{\cos \alpha} \cdot \frac{I_z}{I_y}$$

$$Y = - \tan \alpha \cdot \frac{I_z}{I_y} \cdot Z$$

$$\tan \beta = - \tan \alpha \cdot \frac{I_z}{I_y}$$

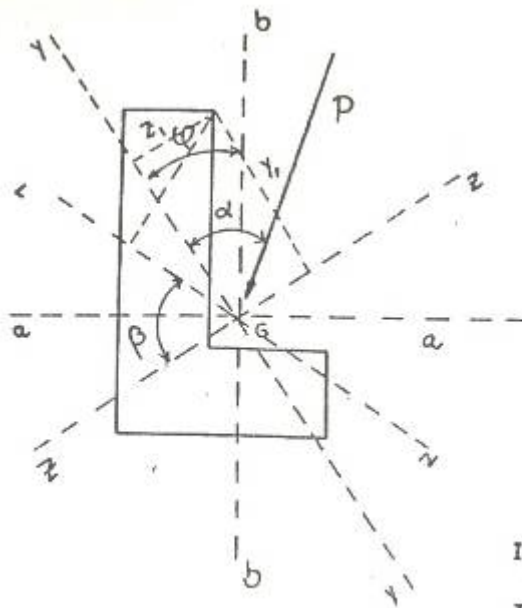
VERIFICACION DE TENSIONES



$$\sigma_c = \frac{M_y \cdot y_1}{I_z} + \frac{M_z \cdot z_1}{I_y} \leq \bar{\sigma}_c$$

$$\sigma_t = \frac{M_z \cdot y_2}{I_z} + \frac{M_y \cdot z_2}{I_y} \leq \bar{\sigma}_t$$

Verificación de Tensiones



- ① DETERM DE G.
- ② DETERM. DE I_{aa} ; I_{bb} ; I_{ab}
- ③ DETERM. EJES Y ; Z (PRINCIPALES)

$$\operatorname{tg} 2\varphi = \frac{2 I_{ab}}{I_a - I_b}$$

- ④ DETERM. I_x ; I_y (PRINCIPALES)

$$I_x = I_b \cos^2 \varphi + I_a \operatorname{sen}^2 \varphi - I_{ab} \operatorname{sen} 2\varphi$$

$$I_y = I_b \operatorname{sen}^2 \varphi + I_a \cos^2 \varphi - I_{ab} \operatorname{sen} 2\varphi$$

- ⑤ DETERM. M_y ; M_x

$$M_y = M \cos \alpha$$

$$M_x = M \operatorname{sen} \alpha$$

- ⑥ DETERM. L M

$$\operatorname{tg} \beta = \frac{I_x \operatorname{tg} \alpha}{I_y}$$

- ⑦ DETERMINACION PUNTOS MAS SOLICITADOS

- ⑧

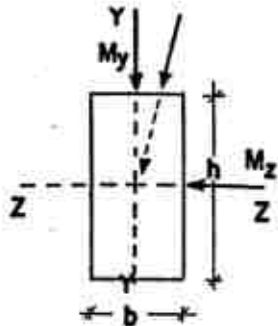
$$\sigma_{\max} = \frac{M_y y_i}{I_x} + \frac{M_x z_i}{I_y} \leq \bar{\sigma}$$

DIMENSIONAMIENTO

$$\sigma = \frac{M_y}{W_z} + \frac{M_z}{W_y}$$

$$\frac{W_z}{W_y} = C$$

$$W_z = \frac{M_y + CM_z}{\bar{\sigma}}$$



SECCIONES RECTANGULARES

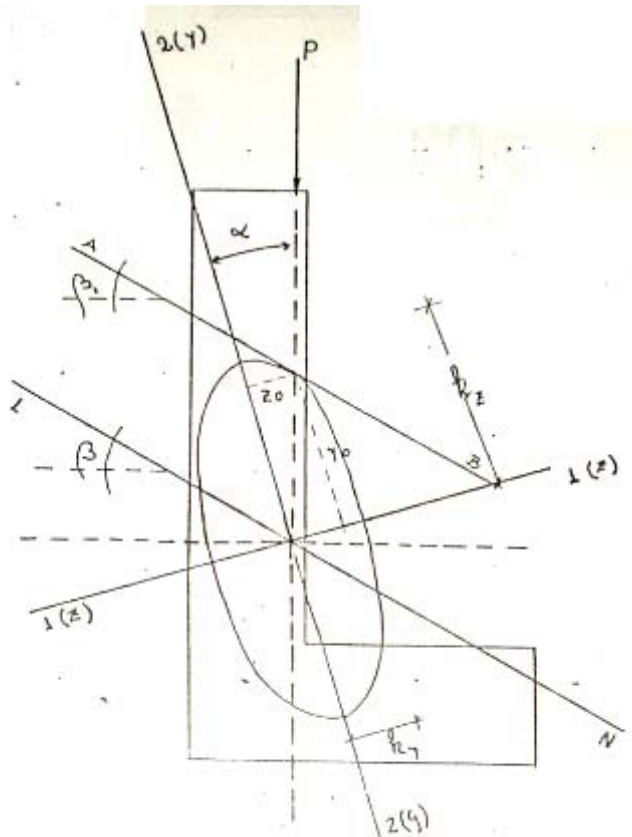
$$C = \frac{W_z}{W_y} = \frac{\frac{b h^2}{6}}{\frac{h b^2}{6}} = \frac{h}{b} = 1.2 ; \dots ; 1.4$$

$$C = \frac{h}{b} = \frac{M_y}{M_z} \quad (\text{SECCION MINIMA}) \quad W_z \approx \frac{z M_y}{\bar{\sigma}}$$

PERFILES LAMINADOS

| | | | | | |
|---|----|---|----|-------|--------|
| [| 12 | a | 16 | | C = 6 |
| | 18 | a | 30 | | C = 7 |
| I | 8 | a | 12 | | C = 7 |
| | 13 | a | 24 | | C = 8 |
| | 25 | a | 34 | | C = 9 |
| | 36 | a | 60 | | C = 10 |

I ALAS ANCHAS 50 a 100 - C = 6 → 13



UTILIZACIÓN DE LA ELIPSE CENTRAL DE INERCIA PARA LA DETERMINACIÓN DE LA LINEA NEUTRA

ECUACION DE LA ELIPSE CENTRAL DE INERCIA :

$$\frac{y^2}{k_x^2} + \frac{z^2}{k_y^2} = 1$$

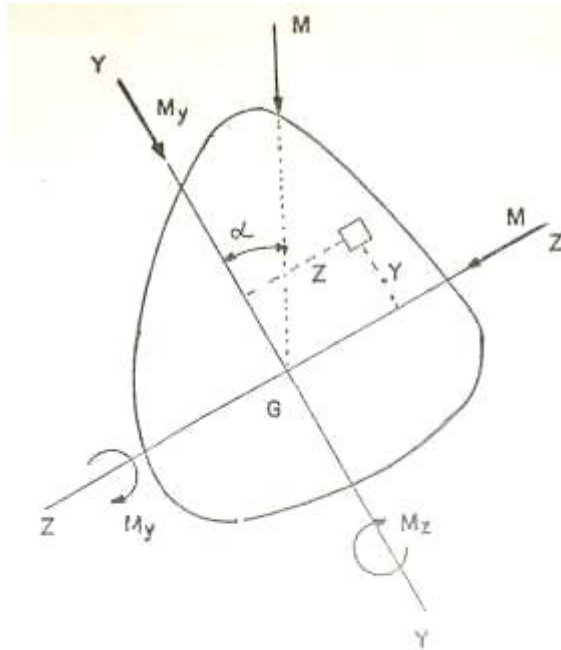
ECUACION DE A B : $\frac{y_0 y}{k_x^2} + \frac{z_0 z}{k_y^2} = 1$

$$\operatorname{tg} \beta_1 = -\frac{B}{A} = -\frac{z_0 k_x^2}{k_y^2 y_0} = \frac{z_0}{y_0} \cdot \frac{I_x}{I_y} = \operatorname{tg} \alpha \cdot \frac{I_x}{I_y}$$

Y COMO LA EC. DE LA LN : $\operatorname{tg} \beta = \operatorname{tg} \alpha \cdot \frac{I_x}{I_y}$

$$\beta = \beta_1$$

EJES BARICENTRICOS CUALQUIERA



$$\int_A \sigma dA = 0$$

$$\int_A \sigma Y dA = M_y$$

$$\int_A \sigma Z dA = M_z$$

$$\sigma = a + bY + cZ$$

$$\int_A \sigma dA = 0 \quad ; \quad \int_A a dA + \int_A bY dA + \int_A cZ dA = 0 \quad ; \quad a = 0$$

$$\int_A \sigma Y dA = M_y \quad ; \quad b \int_A Y^2 dA + c \int_A YZ dA = M_y \quad ; \quad b I_z + c I_{zy} = M_y$$

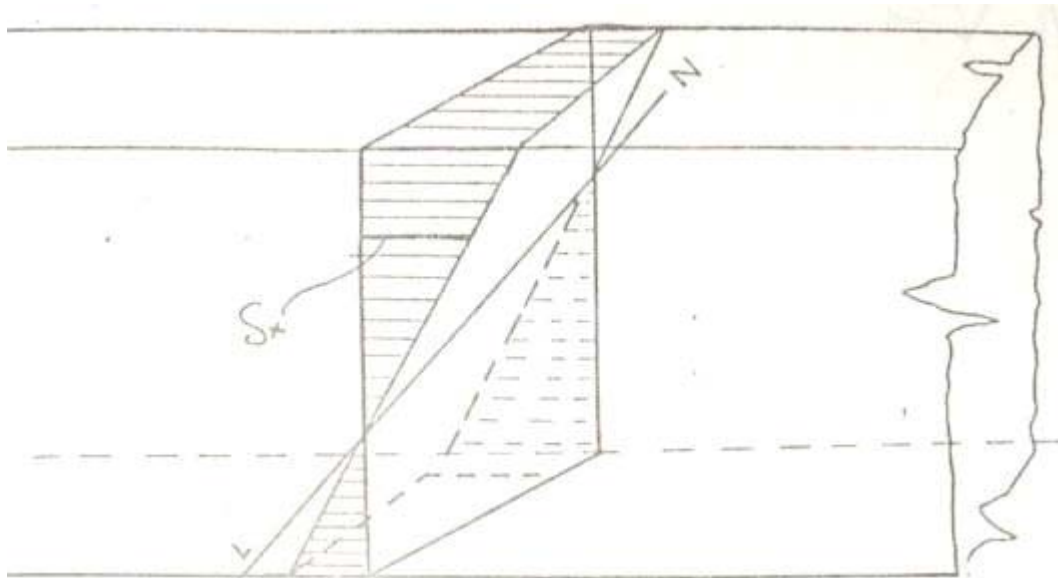
$$\int_A \sigma Z dA = M_z \quad ; \quad b \int_A YZ dA + c \int_A Z^2 dA = M_z \quad ; \quad b I_{zy} + c I_y = M_z$$

$$b = \frac{M_y I_y - M_z I_{zy}}{I_z I_y - I_{zy}^2}$$

$$c = \frac{M_z I_z - M_y I_{zy}}{I_z I_y - I_{zy}^2}$$

$$\sigma = \frac{M_y I_y - M_z I_{zy}}{I_z I_y - I_{zy}^2} \cdot Y + \frac{M_z I_z - M_y I_{zy}}{I_z I_y - I_{zy}^2} \cdot Z$$

FLEXION OBLICUA

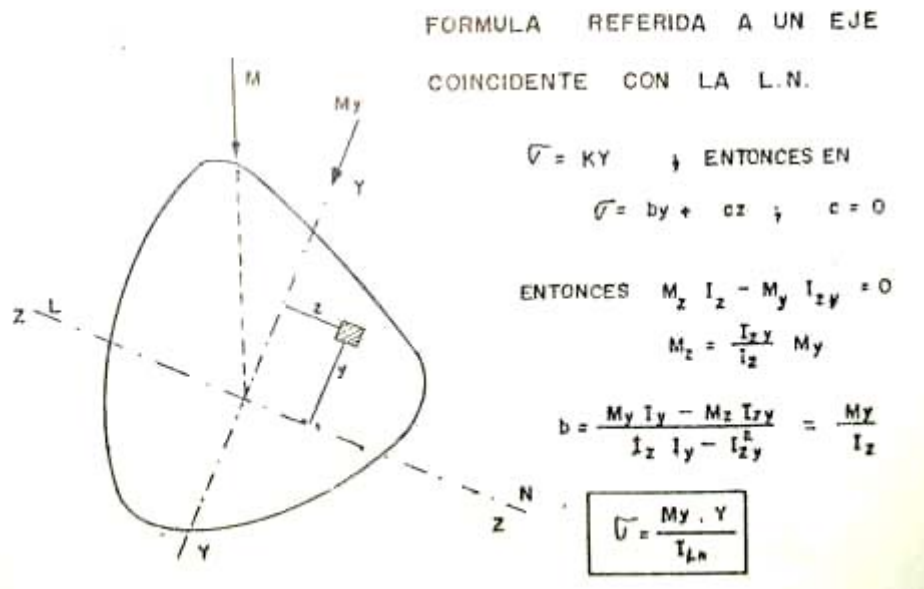
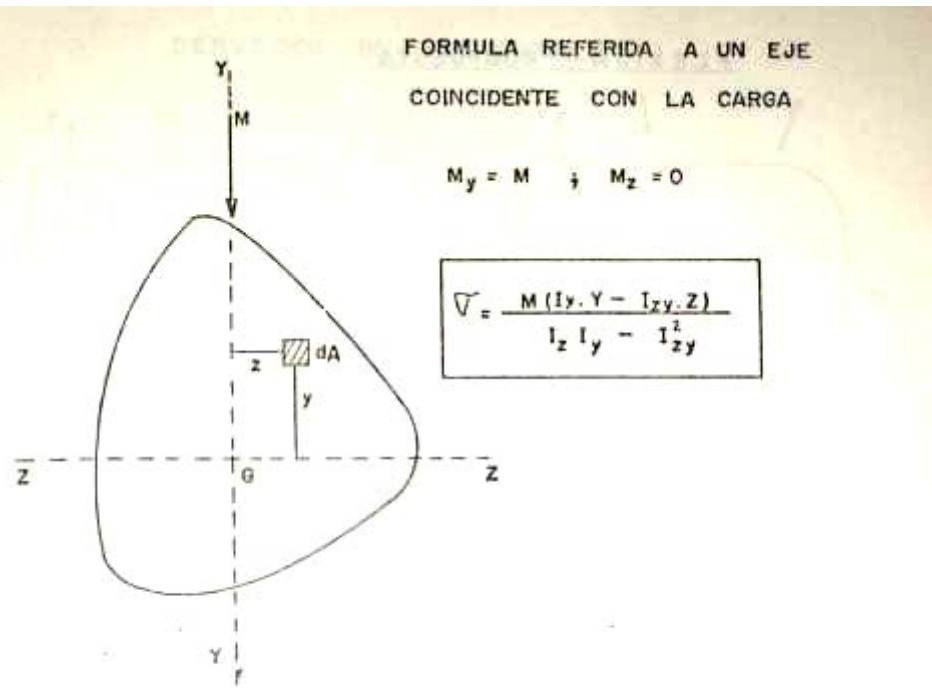


$$\sigma_x = E dX_1 = (K, J) dX_1$$

$$S_x = E dX = (a_1 + b_1 y + c_1 z) dx$$

$$\sigma = \epsilon E = E a_1 + E b_1 y + E c_1 z$$

$$\underline{\sigma = a + b y + c z}$$



Próxima Clase: Flexión oblicua,
línea elástica plana, línea elástica
alabeada

Fin